

Lecture 16

GL Theory

→ Domain Wall Energies

Current in thin wires

Resistance in thin wires

Type-I SC

Normal Conductor

H_c

$h(x)$

$\psi(x)$

Superconductor

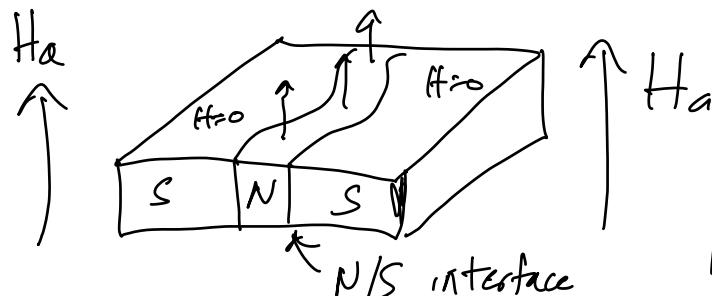
$\lambda_{\text{eff}}(T)$

$\xi_{\text{GL}}(T)$

λ_{eff}

ξ_{GL}

x



Type-I $K \ll 1$

$$K = \frac{\lambda_{\text{eff}}}{\xi_{\text{GL}}}$$

$$\lambda_{\text{eff}} \ll \xi_{\text{GL}}$$

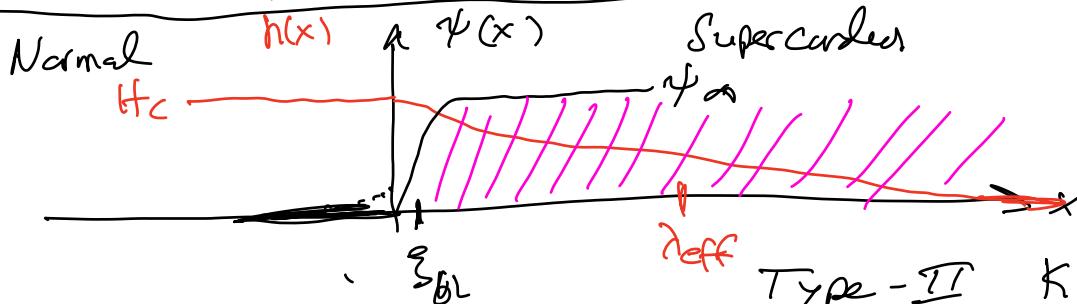
How much energy is
involved in creating the
domain wall.

Positive energy $M_0 H^2 / 2$

paying price

Negative energy $|V|^2$ → losing

$$E_{\text{DW}}^I > 0$$



Type-II $K \gg 1$

$$\lambda_{\text{eff}} \gg \xi_{\text{GL}}$$

Condensation energy is large
and negative

Positive condensation from magnetic screening is small.

$$E_{\text{DW}}^{II} < 0$$

Domain walls proliferate.

Proceed until the quantum limit is achieved. $\Phi = \Phi_0 = h/2e$

Domain Wall Energy

$$\gamma = \frac{\mu_0 H_c^2}{2} S \quad S = \text{width of the domain wall}$$

$\hookrightarrow \gamma/m^2$ Energy per unit area of a domain wall

Excess Gibbs free energy due to the domain wall

$$\delta = \int_{-\infty}^{\infty} \left[\left(1 - \frac{h(x)}{H_c} \right)^2 - \left(\frac{\psi(x)}{\psi_0} \right)^4 \right] dx$$

$h(x)$ = microscopic magnetic field

Normal Metal $h(x) \rightarrow H_c$ $\psi(x) \rightarrow 0$ $1 - \frac{h(x)}{H_c} = 0$
 No contribution to δ integral $(\psi(x)/\psi_0)^4 = 0$

SC $h(x) = 0$ $\psi(x)/\psi_0 = 1$ $1 - 1 = 0$

No contribution to δ integral

$$N \quad h(x) = \begin{cases} H_c e^{-x/\lambda_{\text{eff}}} & x > 0 \\ H_c & x < 0 \end{cases}$$

$$h(x) = \begin{cases} H_c e^{-x/\lambda_{\text{eff}}} & x > 0 \\ H_c & x < 0 \end{cases}$$

$h(x), \psi(x)$ not determined self-consistently

$$\Rightarrow \delta = -\frac{3}{2} \lambda_{\text{eff}} + \frac{25}{24} \sqrt{2} \xi_{GL} \approx \xi_{GL} - \lambda_{\text{eff}}$$

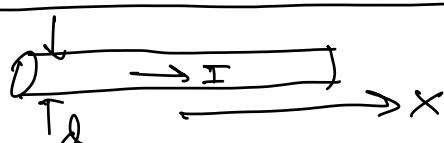
$$\text{Type I} \quad K \ll 1 \quad E_{DW}^{II} > 0 \quad \delta \approx +\frac{25}{24} \sqrt{2} \xi_{GL} = 1.47 \xi_{GL}$$

$$\text{Type II} \quad K \gg 1 \quad \delta \approx -1.5 \lambda_{\text{eff}} \quad E_{DW}^{II} < 0$$

$$\begin{aligned} \text{Exact} \\ \frac{4\sqrt{2}}{3} \xi_{GL} &= 1.99 \xi_{GL} \\ -\frac{8}{3} (\sqrt{2}-1) \lambda_{\text{eff}} \\ &= -1.1 \lambda_{\text{eff}} \end{aligned}$$

$$\text{Boundary} \quad \delta = 0 \quad \Rightarrow \quad K = \frac{25\sqrt{2}}{36} = 0.98$$

$$\text{Exact Result} \quad K = \frac{1}{\sqrt{2}} \approx 0.7$$



Current Flow in a
Thin SC Wire

Thin short wire
 T

$D \ll \xi_{GL}$ $\psi(x)$ does not vary
over the diameter of the wire

↪ Short compared to $\xi_{02} \rightarrow$ No variation of $\psi(x)$ along x

$$\psi(x) = |\psi(x)| e^{i\phi(x)}$$

↪ $|\psi(x)|$ is a constant

$$\bar{J} = \frac{e^*}{m^*} |\psi|^2 (h\nabla\phi - e^* \vec{A})$$

$$= e^* |\psi|^2 \vec{v}_s$$

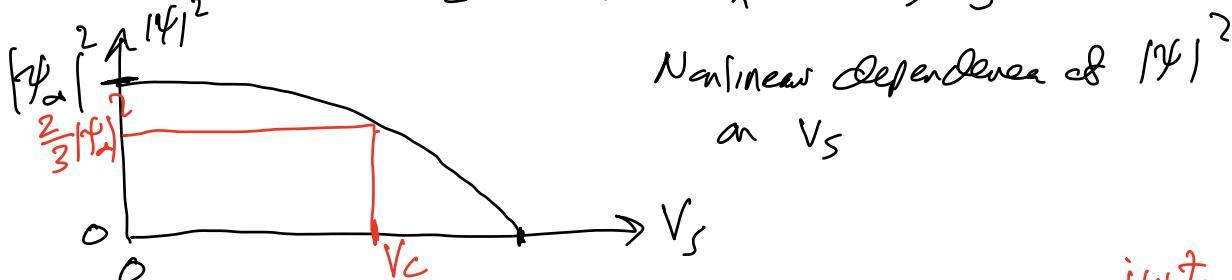
$$f_s - f_n = \alpha |\psi|^2 + \frac{\rho}{2} |\psi|^4 + \frac{1}{2} m^* v_s^2 |\psi|^2 + \frac{\mu_0 H^2}{2}$$

$$\frac{\partial(f_s - f_n)}{\partial |\psi|} = 0 = 2\alpha |\psi| + 2\rho |\psi|^3 + m^* v_s^2 |\psi| = 0$$

$$|\psi|^2 = -\frac{\alpha}{\beta} \left(1 - \frac{m^*}{2(\alpha)} v_s^2 \right)$$

$$|\psi_\alpha|^2 = \frac{\alpha}{\beta} \quad g_{02}^2 = \frac{\hbar^2}{2m^* \alpha}$$

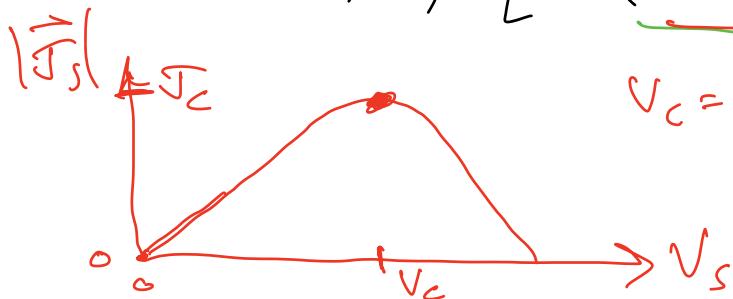
$$|\psi|^2 = |\psi_\alpha|^2 \left[1 - \left(\frac{m^* \xi_{02}(T)}{\hbar} v_s \right)^2 \right]$$



$$\bar{J}_s = e^* |\psi|^2 \vec{v}_s$$

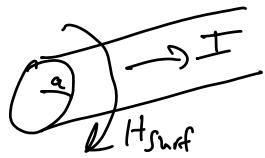
$$= e^* |\psi_\alpha|^2 \left[1 - \left(\frac{m^* \xi_{02}(T)}{\hbar} v_s \right)^2 \right] \vec{v}_s$$

3w



$$\frac{\partial \bar{J}_S}{\partial V_f} = 0 \Rightarrow V_C^2 = \frac{e^2}{(2m^*)^2 \bar{J}_{SL}^2}, \quad J_c = \left(\frac{2}{3}\right)^{3/2} \frac{H_c}{\lambda_{eff}}$$

Silsbee's Rule



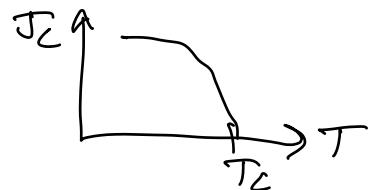
$$H_{Surf} = \frac{I}{2\pi a}$$

$$\Rightarrow H_c = \frac{I_c}{2\pi a}$$

$$J_c = \frac{I_c}{2\pi a \lambda_{eff}}$$

$$J_c = \frac{H_c(\tau)}{\lambda_{eff}(\tau)}$$

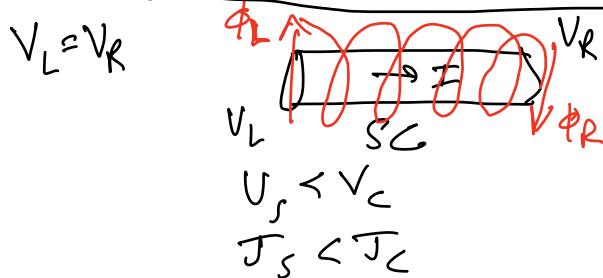
$$J_c \sim (1-t)^{3/2} \text{ near } T_c$$



How does resistance develop in a thin SC wire?

$$\bar{J}_S = \frac{e^*}{m^*} |\psi| \left(\frac{\hbar \nabla \phi}{\lambda} \right)$$

$$\psi = |\psi| e^{iqx}$$



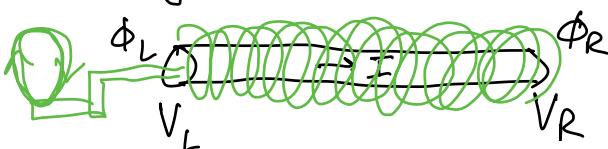
Phase helix bar pitch $\frac{2\pi r}{q}$

Fixed \bar{J}_S , fixed I

Fixed $\phi_R - \phi_L$

Zero resistance

To get resistance there has to be a voltage drop.



$$V = V_R - V_L \neq 0$$

Josephson Relation AC Josephson Equation

$$\frac{d(\phi_R - \phi_L)}{dt} = \frac{2e}{h} V$$

"Turn the crank" to add phase winding to the wire at a constant rate.

$$V > 0, \bar{E} \neq 0 \quad \bar{E} = \frac{\partial (\Lambda \bar{J}_S)}{\partial t} \Rightarrow \frac{\partial N_S}{\partial t} = \frac{eE}{m}$$

$E \neq 0 \Rightarrow V_S$ must increase.

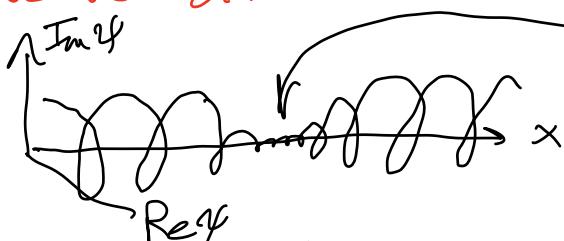
V_S is limited by V_C .

Dilemma as more phase windings are added.

$$\bar{J}_S \sim |\chi(x)|^2 \frac{\partial \phi}{\partial x} = \text{constant} \propto 1$$

↳ limited by V_C
↳ limited

Resolve the dilemma : Create a phase-slip center



Make $|f(x)| \rightarrow 0$ in some small region

Dissolve phase windings in units of 2π .

Fluctuation Phenomena

Heat Bath Borrow $\hbar \beta T$ of energy $T \approx T_C$

$$\Delta F_0 = \frac{8\sqrt{2}}{3} \mu_0 H_c^2 (A \oint_{6L})$$

cross sectional area of wire

cost to create the fluctuation

$\Delta F_0 \rightarrow 0$ as $T \rightarrow T_C$
 $\sim (1-t)^{1/2}$

$$R \sim \underset{I \rightarrow 0}{L} \frac{V}{I} = \frac{\pi h^2 R}{2e^2 \hbar \beta T} e^{-\Delta F_0 / \hbar \beta T}$$

L AMH

Langer, Ambegaokar, McCumber, Halperin

